## Complete Coverage Navigation for Autonomous Clay Roller in Salt-Farming Application

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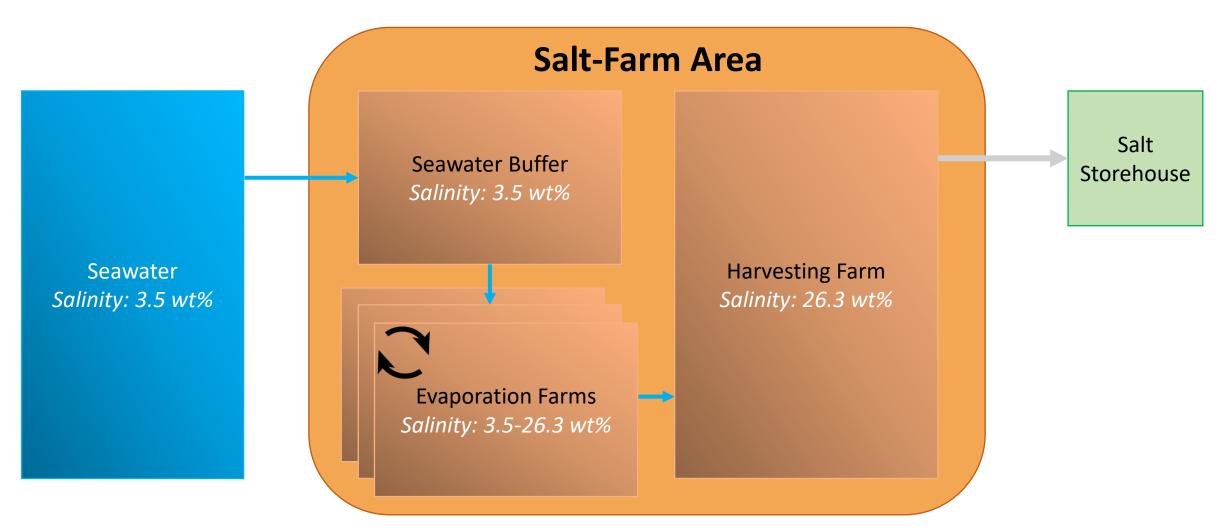


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## Background

- Basic of salt-farming process in Thailand
- Why do we need to smoothen our farm?
- A tool to ease on roughness problem: Clay Roller

### Basic of salt-farming process in Thailand



### Why do we need to smoothen our farm?

Currently, salt-gathering are performed by a farmer stepping their feet to the farm field which causes an *order of roughness* in the farm field.

Neglecting this problem leads to...

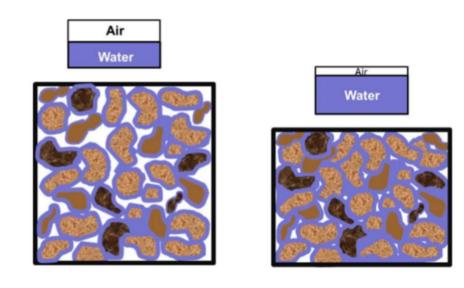
- slowness of the evaporation rate
- inferior salt quality for the next agricultural cycle

### Clay Roller

Nowadays, we used *Clay Roller* for rolling over and over on the clay farm field. (and farmers are still driving it.)



This makes the clay *tighter* and *smoother* which is more ideal for salt-farming.



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### "Complete Coverage Navigation-type" Mobile Robot

### **Deterministic Navigation**

- Certain converging time
- Predictable behavior

#### **Random Navigation**

- -Uncertain complete coverage converging time.
- -Widely used in differential drive kinematics.
- -Unpredictable behavior

### Scope of this work

#### Path Planner aka. global\_planner

- Plan the overall complete coverage path that suits with "Bicycle Kinematics"

#### Path Tracker aka. local\_planner

- Control the clay roller to follow the generated path.

### Not in this scope of work

### Low Level Control (for controlling steering angle and driving speed)

- Hardware-Level PID controller has been done

#### Localization

- System is assumed to use RTK which provided 5 cm. of accuracy.

## Rear-Steering Kinematics Fundamental

Most literatures describes about *front-steering* bicycle model



### Continuous Kinematics of Rear Steering Bicycle Model

According to rolling constraint to the front wheel and the sliding constraint from both wheels, we obtains

$$\begin{bmatrix} \sin\left(\frac{\pi}{2}\right) & -\cos\left(\frac{\pi}{2}\right) & 0 \\ \cos\left(\frac{\pi}{2}\right) & \sin\left(\frac{\pi}{2}\right) & 0 \\ \cos\left(\frac{\pi}{2} + \delta\right) & \sin\left(\frac{\pi}{2} + \delta\right) & L\sin\left(-\frac{\pi}{2} + \delta\right) \end{bmatrix} \begin{bmatrix} \dot{x}_R \\ \dot{y}_R \\ \dot{\theta} \end{bmatrix} = \begin{bmatrix} r\dot{\phi} \\ 0 \\ 0 \end{bmatrix} \quad (1)$$

$$\begin{bmatrix} \dot{x}_R \\ \dot{y}_R \\ \dot{\theta} \end{bmatrix} = r\dot{\varphi} \begin{bmatrix} 1 \\ 0 \\ -\frac{\tan \delta}{L} \end{bmatrix} \tag{2}$$

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{\theta} \end{bmatrix} = r\dot{\varphi} \begin{bmatrix} \cos\theta & -\sin\theta & 0 \\ \sin\theta & \cos\theta & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \\ -\frac{\tan\delta}{L} \end{bmatrix}$$
(3)

$$\begin{bmatrix} \dot{x}_I \\ \dot{y}_I \\ \dot{\theta} \end{bmatrix} = r\dot{\phi} \begin{bmatrix} \cos\theta \\ \sin\theta \\ -\frac{\tan\delta}{L} \end{bmatrix}$$
 (4)

\*The frame position is at the middle of front wheel axle.

[1] I. R. N. a. D. S. Roland Siegwart, Introduction to Autonomous Mobile Robots, London: The MIT Press, 2011.

### Discrete Kinematics of Rear Steering Bicycle Model

$$\begin{bmatrix} \dot{x}_{I} \\ \dot{y}_{I} \\ \dot{\theta} \end{bmatrix} = r\dot{\phi} \begin{bmatrix} \cos\theta \\ \sin\theta \\ \tan\delta \\ -\frac{\tan\delta}{L} \end{bmatrix}$$

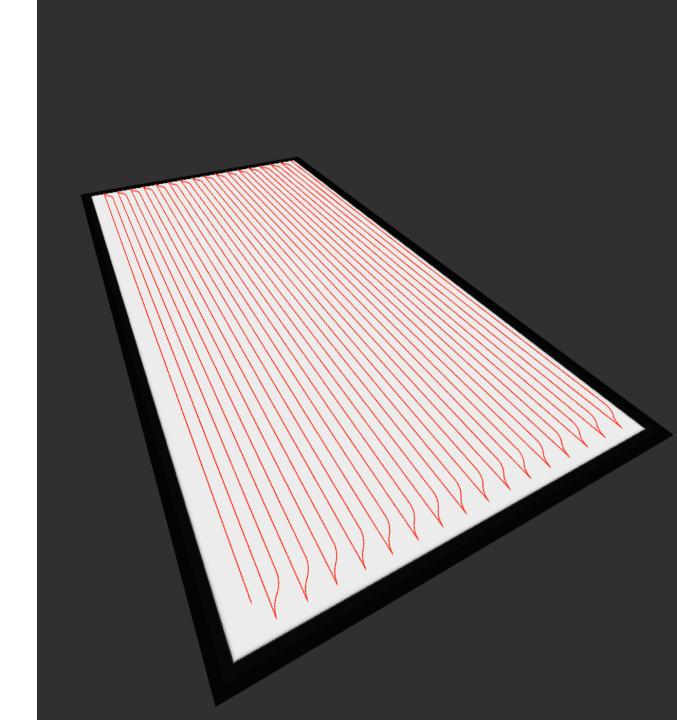
$$\dot{x} = \Delta x/\Delta t$$

$$\begin{bmatrix} \Delta x_{I} \\ \Delta y_{I} \\ \Delta \theta_{I} \end{bmatrix} = r\Delta\phi \begin{bmatrix} \cos\theta \\ \sin\theta \\ \tan\delta \\ -\frac{\tan\delta}{L} \end{bmatrix}$$
(5)

$$\begin{bmatrix} x_I(n+1) \\ y_I(n+1) \\ \theta_I(n+1) \end{bmatrix} = \begin{bmatrix} x_I(n) \\ y_I(n) \\ \theta_I(n) \end{bmatrix} + r\Delta\phi \begin{bmatrix} \cos\theta \\ \sin\theta \\ \tan\delta \\ -\frac{\tan\delta}{L} \end{bmatrix}$$
 (6) This form will be used in **Path Planner**

## Complete Coverage Path Planner

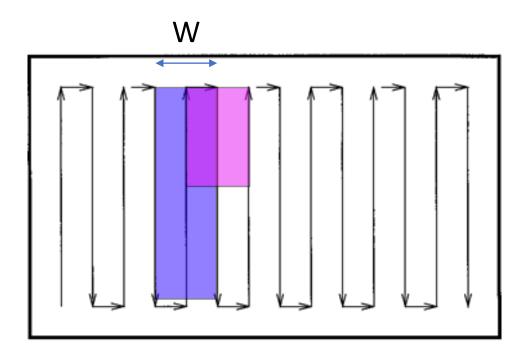
- Path Modification
- Costmap and Thresholds
- Overlapping Angle and Turning Angle
- Algorithm Flowchart



### Path Modification from Back-and-forth Motion

Normal **back-and-forth\*** path doesn't suit Initial Pose with bicycle kinematic, path modification is, therefore, applied to *every corner*. Final Pose

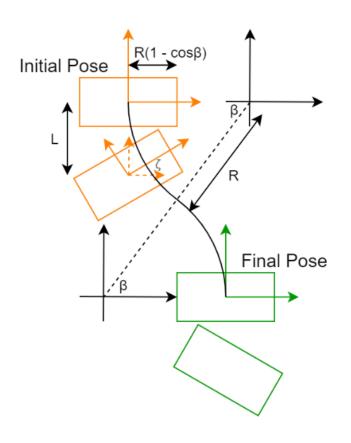
### Overlapping Number



In this example, 
$$\Delta y^R = \frac{W}{2}$$
, therefore,  $\eta = 2$ 

$$\eta = \frac{W}{\Delta y^R} \tag{7}$$

### Turning Angle



$$\eta = \frac{W}{\Delta y^R} \tag{7}$$

According to the geometry,

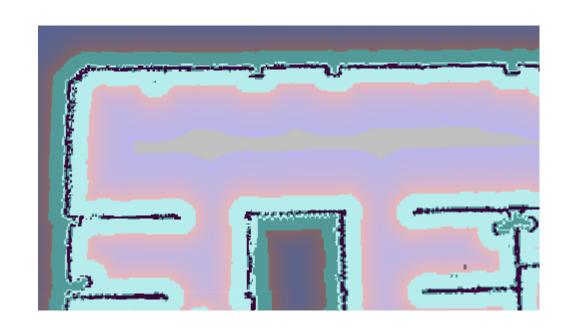
$$R = L \cot \delta_{max} \tag{8}$$

$$\Delta y^R = 2R(1 - \cos \beta). \tag{9}$$

From (7), (8), and (9) we could conclude that

$$\beta = \cos^{-1}\left(1 - \frac{W}{2\eta L \cot \zeta_{max}}\right) \quad (10)$$

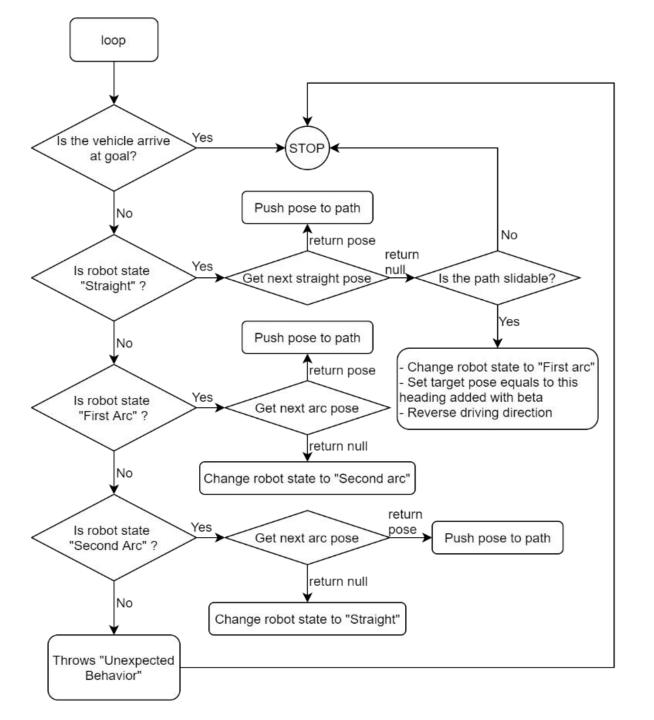
### Inflation Costmap and Thresholds



It represents the cost (difficulty) of traversing different areas of the map

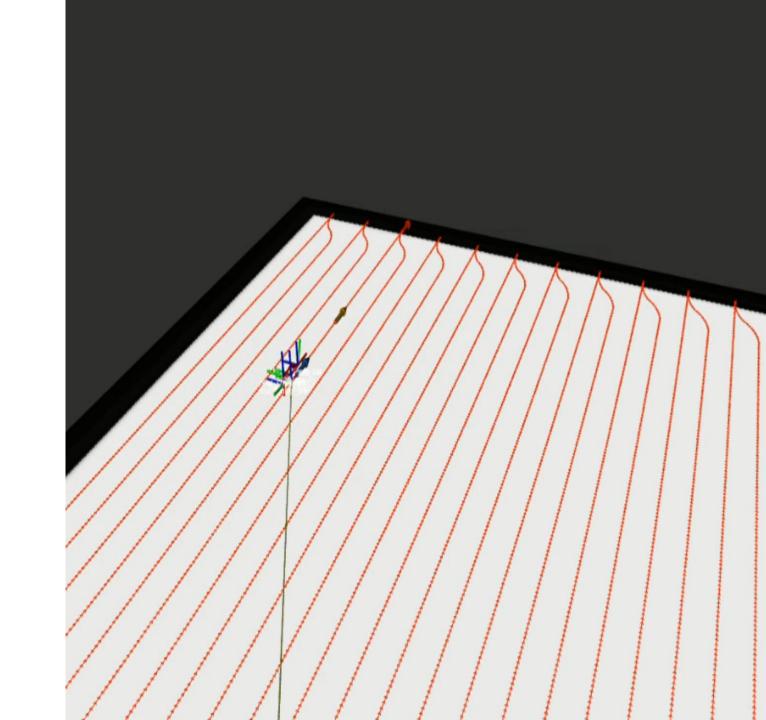
In the program procedure, the operation could be depended on the costmap value of that position

## (Simple) Algorithm Flowchart



# Complete Coverage Path Tracker

- Turning Edge Detector
- Steering Control with Pure Pursuit
- Driveline Control with Trapezoidal Velocity Profile
- Supervisor

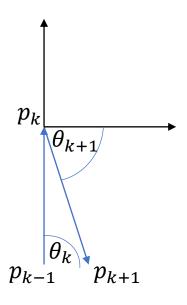


### Turning Edge Detector

A detector is used to detect edges of the generated path to inform other modules.

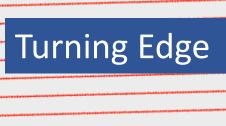
$$p_{edge} = \begin{bmatrix} x_{edge} \\ y_{edge} \end{bmatrix}$$

$$\Delta p_k = p_k - p_{k-1} = \begin{bmatrix} \Delta x_k \\ \Delta y_k \end{bmatrix}$$



$$p_{edge} = \left\{ p_k \ such \ that \ \left| \operatorname{atan} \left( \frac{\Delta y_{k+1}}{\Delta x_{k+1}} \right) - \operatorname{atan} \left( \frac{\Delta y_k}{\Delta x_k} \right) \right| \ge \frac{\pi}{2} \right\}$$

$$p_{edge} = \left\{ p_k \text{ such that } |\theta_{k+1} - \theta_k| \ge \frac{\pi}{2} \right\}$$



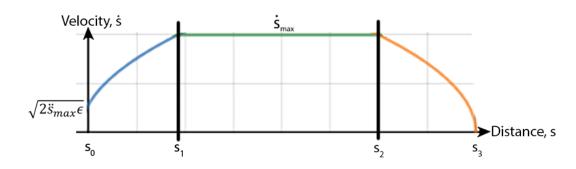
### Driveline Control with Trapezoidal Velocity Profile

This controller is based on a simple equation of motion:

$$\dot{s}^{2}(t) = \dot{s}^{2}(0) + 2\ddot{s}_{max}s(t) \qquad \qquad \dot{s}(s) = \sqrt{\dot{s}^{2}(0) + 2\ddot{s}_{max}s}$$

This control law is feasible due to the fact that we've a control authority over  $\dot{s}(s)$ .

$$\dot{s}(s) = \begin{cases} \sqrt{2\ddot{s}_{max}(s - s_0 + \epsilon)} & ; \ s_0 \le s < s_1 \\ \dot{s}_{max} & ; \ s_1 \le s \le s_2 \\ \sqrt{2\ddot{s}_{max}(s_3 - s)} & ; \ s_2 < s \le s_3 \end{cases}$$



 $s_0$  is the start position of a lane. where

 $s_3$  is the end position of a lane (turning edge)

$$s_1 = s_0 + \frac{\dot{s}_{max}^2}{2\ddot{s}_{max}} - \epsilon$$
 (the position when it stops accelerating)  
 $s_2 = s_3 - \frac{\dot{s}_{max}^2}{2\ddot{s}_{max}}$  (the position when it starts decelerating.)

$$s_2 = s_3 - \frac{\dot{s}_{max}^2}{2\ddot{s}_{max}}$$
 (the position when it starts decelerating.

### Steering Control with Pure Pursuit

1) Obtain target point robot frame,  $p_T^R$  from

$$p_T^R = T_W^R p_T^W$$

where 
$$T_W^R = \begin{bmatrix} \cos(\varphi) & \sin(\varphi) & -x_R^W \cos(\varphi) - y_R^W \sin(\varphi) \\ -\sin(\varphi) & \cos(\varphi) & x_R^W \sin(\varphi) - y_R^W \cos(\varphi) \\ 0 & 0 & 1 \end{bmatrix}$$
  $T_R^W$  is the target point in robot(clay roller) frame  $T_R^W$  is the transformation from robot frame to world frame  $T_R^W$  is the path curvature

2) Obtain the path curvature,  $\gamma$ , from

$$\gamma = \frac{2y_T^R}{l^2},$$

3) Obtain the target steering angle,  $\delta$ , from

$$\delta = \tan^{-1}(-\gamma L).$$

### Nomenclature

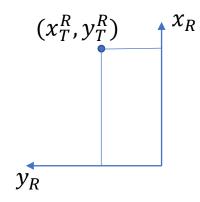
 $p_T^W$  is the target point in world frame

 $p_T^R$  is the target point in robot(clay roller) frame

 $\gamma$  is the path curvature

l is the lookahead distance

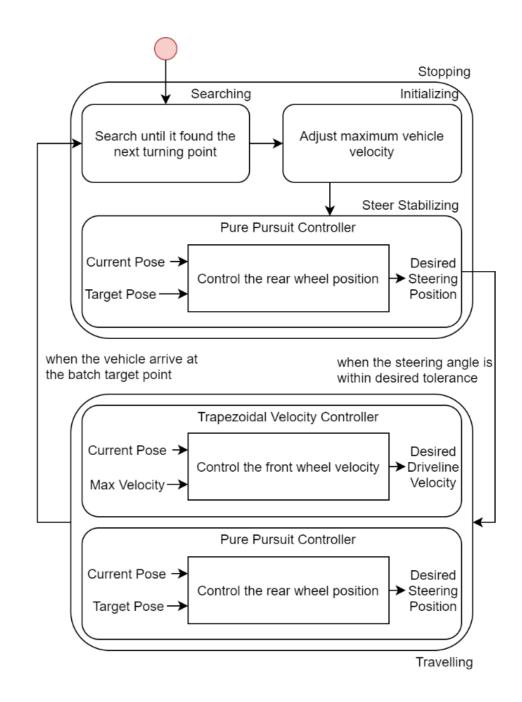
 $\delta$  is the target steering angle

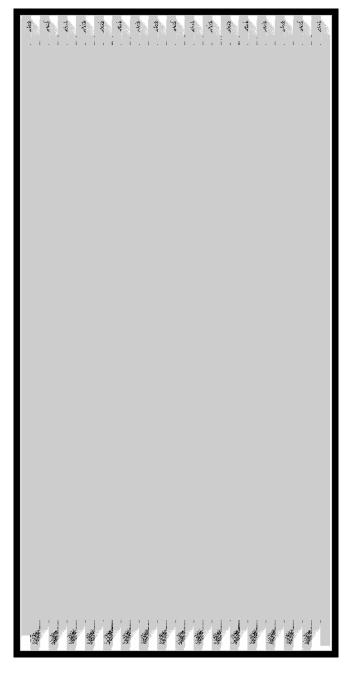


### Supervisor

A state machine with 4 states

- 1) Searching
- 2) Initializing
- 3) Steer Stabilizing (Optional)
- 4) Travelling





## Results

Path Planner

Area Coverage: 97.3%

Path Tracker

Area Coverage: 95.8%

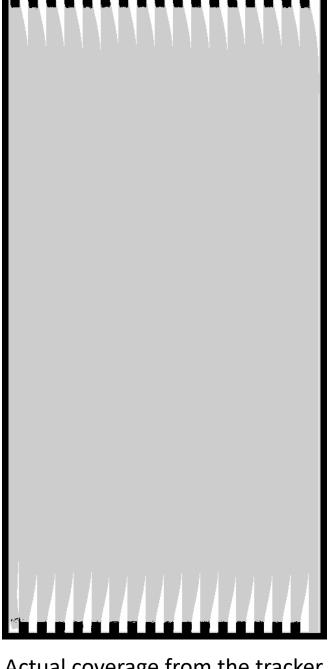
Time Consumed: 34 min.

Table I: Planner Configurations

Parameter Name	Value
Step Size	0.2 meters
Overlapping Number	1
Maximum Steering Angle	0.5 radians
Sliding Stop Threshold	50
Straight Pausing Threshold	2
Stopping Bound	1.5 meters
Initial Position	(-46.5, 23.8)

Table II: Tracker Configurations

Parameter Name	Value
Minimum Velocity	0.1 meters/second
Maximum Velocity	1.0 meters/second
Maximum Acceleration	0.1 meters/second^2
Lookahead distance	5.0 meters
Distance Tolerance	0.2 meters



Actual coverage from the tracker

Predicted coverage from the planner

### Conclusion

• The foundation of Complete Coverage Navigation could be formed from existing simple algorithms.

• This **Path Planner** missed 2.7% of the farm-field area.

• This **Path Tracker** missed 1.6% of the planned area while its travelling is within 34 minutes.

### Thank you for your attention

## Q&A Session

For further inquiries, contact me at

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